

**Microwave Engineering I**

**Final**

**April 29, 2002**

Name Kay

SS# \_\_\_\_\_

You may use your portfolio and a calculator.

**Grading:**

You will receive the highest of....

Midterm I      OR      Final Problems 1 and 2

Midterm II     OR      Final Problems 3 and 4

Midterm III    OR      Final Problems 5 and 6

Good luck and do well!

**Problem 1 (50 points) Smith Charts, Lossy Lines, Double Stub Matching**

(a) An antenna has an impedance of  $25 + j 10 \Omega$ . It is connected to a  $50 \Omega$  line that is 1 meter =  $2.125 \lambda$  long. The line has a loss factor of  $\alpha = 2 \text{ Np/m}$ . What is the input impedance to this line?

(b) Design a double stub matching network for a load that is  ~~$10 - j 10 \Omega$~~   $35 + j 5 \Omega$ . Stubs are parallel, short circuited lines. The distance between the two stubs is  $0.125 \lambda$ . All lines are  $50 \Omega$ .

$$(a) Z_L = 25 + j 10 \Omega / 50 \Omega = 0.5 + j 0.2$$

$$e^{-2\alpha z} \uparrow \uparrow = 0.2$$

$z = 1 \text{ m}$

$$Z_{in} = (1.05 + j 0.15) 50 \Omega = 52.5 + j 7.5 \Omega$$

$$(b) Z_L = \frac{35 - j 5 \Omega}{50 \Omega} = 0.7 - j 0.1 \quad \text{Draw circle } 0.125 \text{ TWG}$$

$$\text{Convert to } Y_L = 1.4 - j 0.2$$

$$\text{Follow real circle to } Y_A = 1.4 + j 0.1$$

Rotate TWG to matching

$$\text{circle } Y_B = 1.0 - j 0.325$$

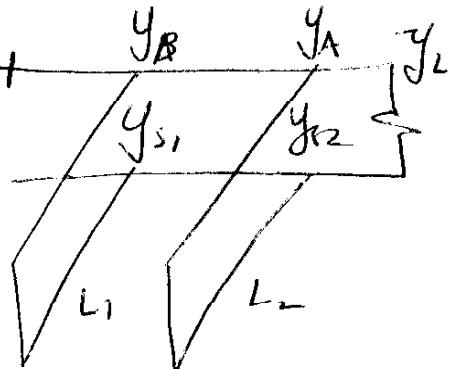
$$1 + j 0 = Y_{S1} + Y_B \Rightarrow Y_B = j 0.325$$

$$Y_A = Y_{S2} + Y_L \Rightarrow Y_{S2} = j 0.3$$

Rotate  $y_{S1}$  TWL to  $y_{S2}$

$$L_1 = 0.25 - 0.05 = 0.2 \lambda$$

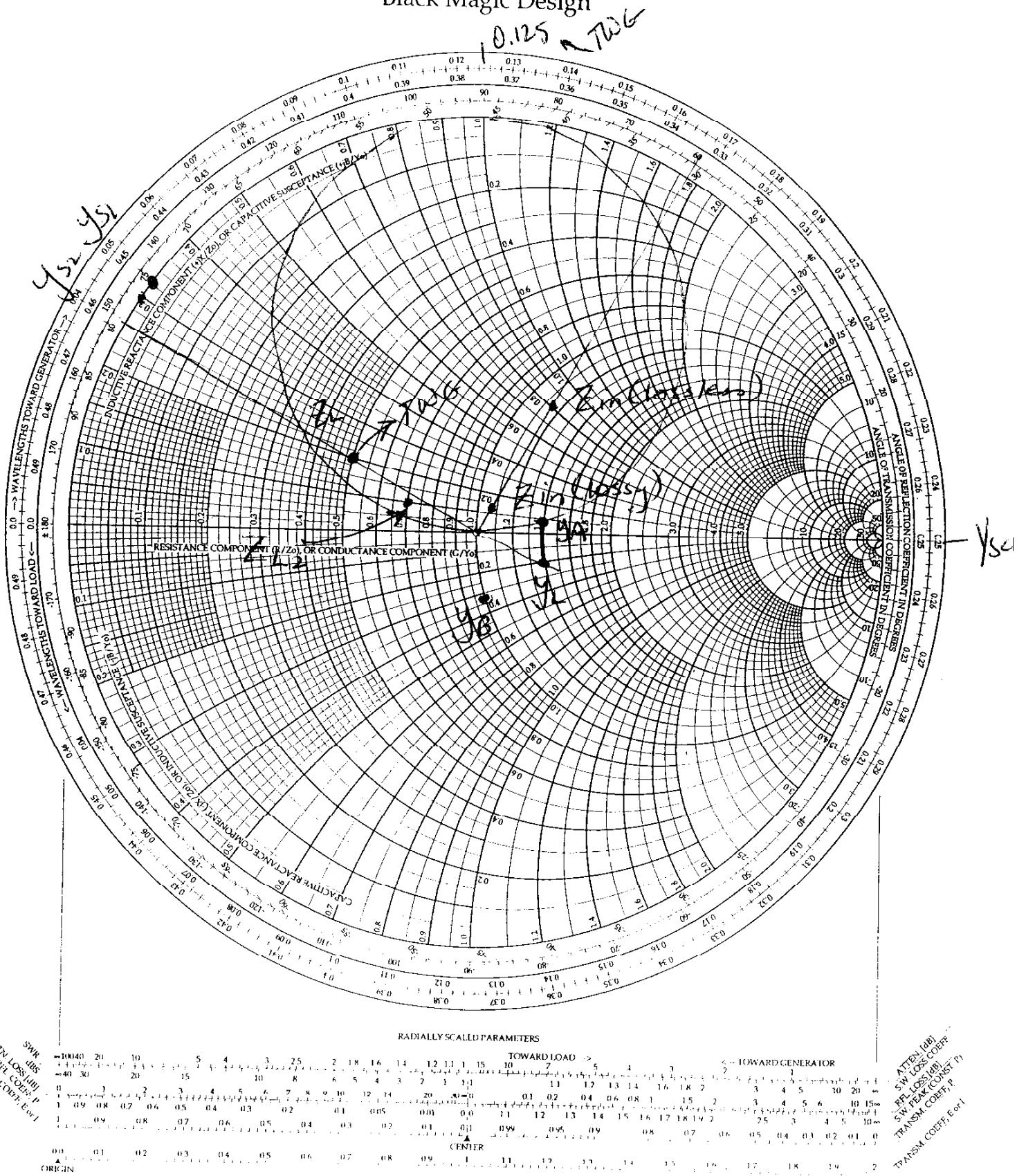
$$L_2 = 0.25 - 0.048 = 0.22 \lambda$$



# The Complete Smith Chart

Problem 1

Black Magic Design



### Problem 2 (50 points) Steady State Transmission Lines

A  $50 \Omega$  transmission line is fed by a 1V sinusoidal generator that has an impedance of  $25 \Omega$ . The line is  $0.3 \lambda$  long. The load is  $200 - j 10 \Omega$ .

- Find the voltage standing wave ratio on the line.
- Write an expression for the positive traveling CURRENT on the line.
- Write a TIME DOMAIN expression for the TOTAL VOLTAGE on the line.

Note: If you do not have time to compute the complex values involved in this problem, write expressions for the items that you would use, including the values of all variables.

$$(a) Z_L = \frac{200 - j 10}{50} = 4 - j 0.2$$

$$\boxed{VSWR = 4.0}$$

$$(b) Z_{in} = (0.26 + j 0.3) 50 \Omega =$$

$$110 = V_g \left( \frac{Z_g = 25 \Omega}{Z_{in}} \right) Z_{in} \quad V_{in} = \frac{Z_{in}}{Z_{in} + Z_0} V_g =$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{4 - j 0.2 - 25}{4 - j 0.2 + 25} \quad V_{in} = V_o^+ e^{-j\beta L} + \Gamma_L V_o^+ e^{+j\beta L}$$

$$V_o^+ = \frac{V_{in}}{e^{-j\frac{2\pi}{\lambda} 0.3\lambda} + \Gamma_L e^{+j\frac{2\pi}{\lambda} 0.3\lambda}}$$

$$\boxed{I_o^+ = \frac{V_o^+}{Z_0} =}$$

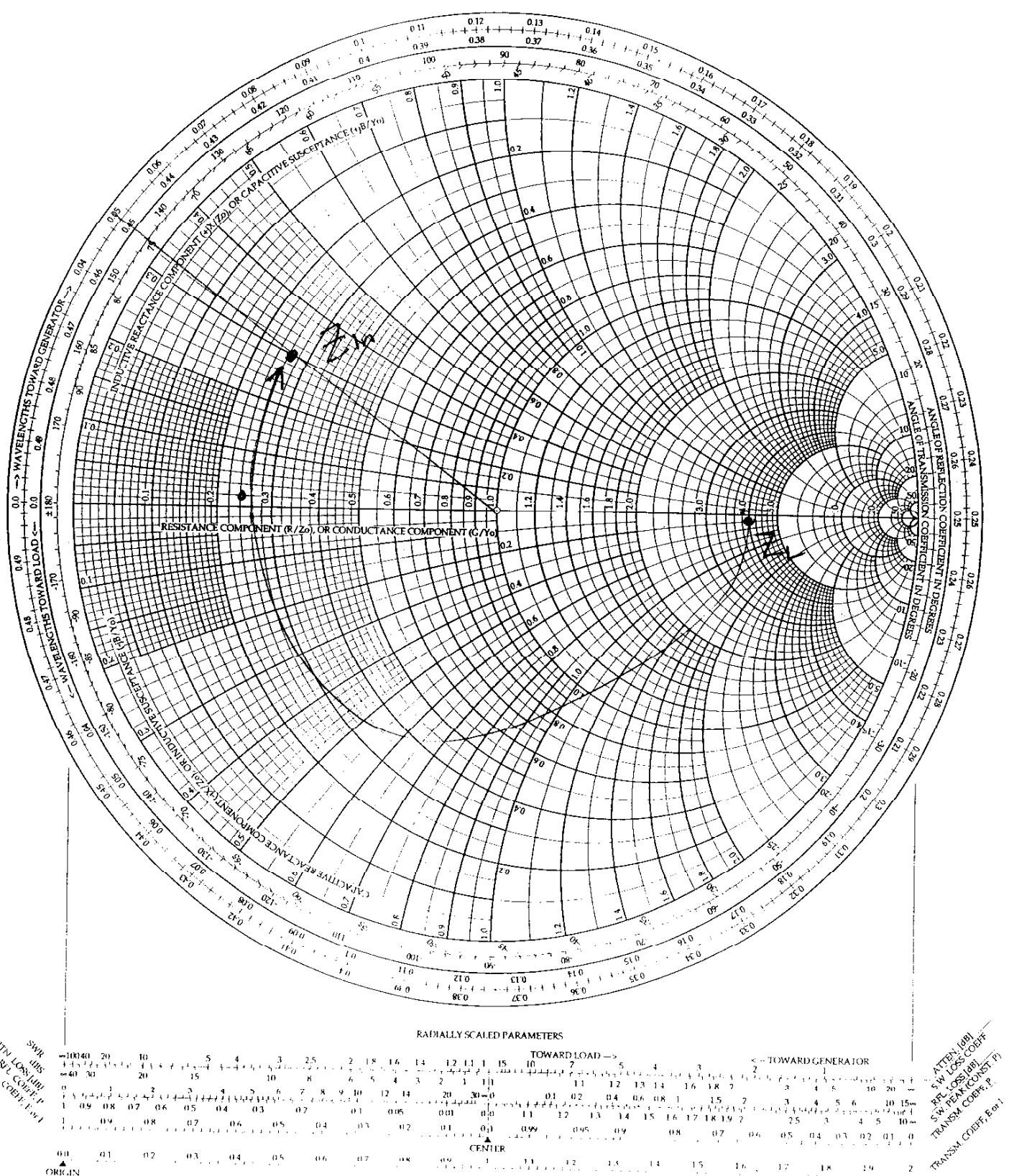
$$\tilde{V}(z) = V_o^+ e^{-j\beta z} + \Gamma_L V_o^+ e^{+j\beta z}$$

$$V(z, t) = |V_o^+| \cos(\omega t - \beta z + \phi_{V_o^+})$$

$$+ |\Gamma_L| |V_o^+| \cos(\omega t + \beta z + \phi_{V_o^+} + \phi_{\Gamma_L})$$

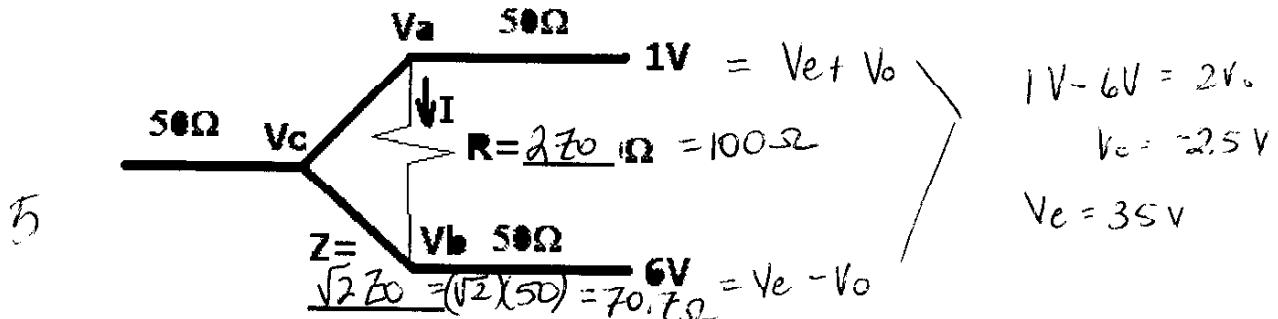
# The Complete Smith Chart

## Black Magic Design



### Problem 3 (50 points) Couplers and Power Dividers

- (a) Design a Wilkinson power divider for equal power combining. All input and output lines are  $50\Omega$ . Specify R and Z below.



- (b) If the input voltages are 1 V and 6 V, find:

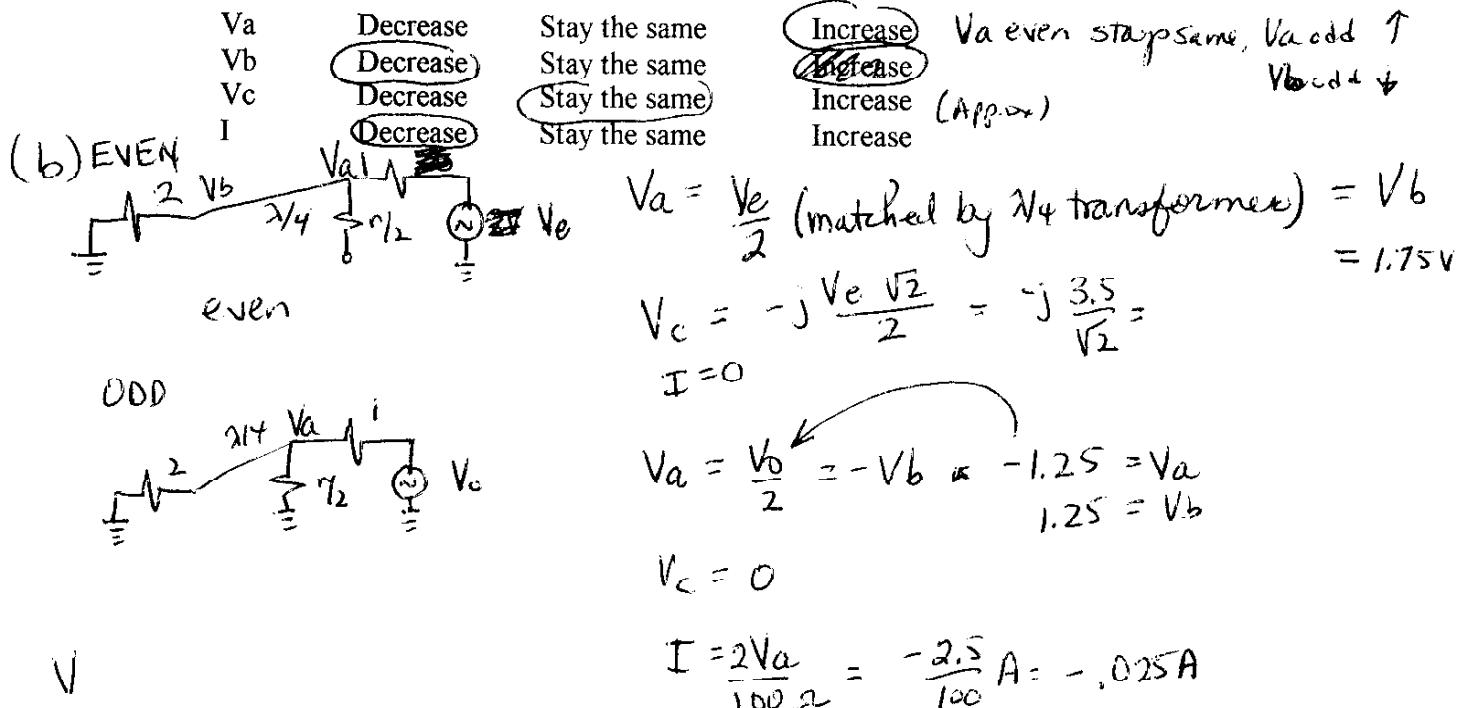
$$10 \quad V_a = \underline{\hspace{2cm}} \text{ V} = 1.75 + -1.25 = 0.5$$

$$10 \quad V_b = \underline{\hspace{2cm}} \text{ V} = 1.75 + 1.25 = 3$$

$$10 \quad V_c = \underline{\hspace{2cm}} \text{ V} = -j \frac{3.5}{\sqrt{2}} + 0 =$$

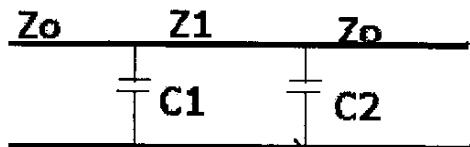
$$10 \quad I = -\underline{.25} \text{ mAmps} = 0 - .025 \text{ A}$$

- (c) If a mistake is made in manufacturing, and a resistor that is twice as large as it should be ( $=2R$ ) is installed, what will happen to each value?



### Problem 4 (50 points) Filters

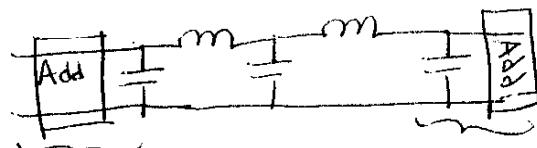
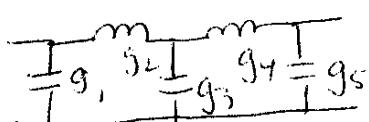
- Find the normalized coefficients ("g" values) for a maximally flat low pass filter that has a cutoff frequency of 1 GHz and passes less than -40 dB at 3 GHz.
- Demonstrate how to apply the Kuroda identities to this filter design. Numerically compute the values of one of the identities, and demonstrate the rest simply by drawing them.
- Show how to implement the system below using open circuited stubs.



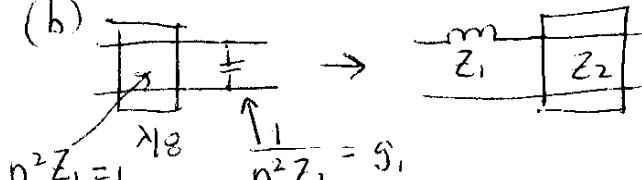
(a) From Fig 8.26 p 450  $| \frac{\omega}{\omega_c} | - 1 = | \frac{3}{1} | - 1 = 2.0$

For 40 dB, you need a 5<sup>th</sup> order filter. From Table 8.3 p 449  
 $g_1 = 0.6180, g_2 = 1.6180, g_3 = 2, g_4 = 1.6180, g_5 = 0.6180, g_6 = 1.0$

(b)



(b)



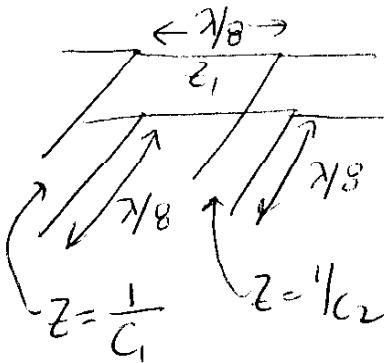
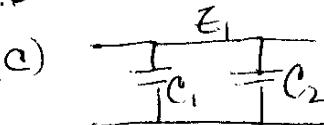
$$n^2 Z_1 = 1 \quad \lambda/8 \quad \frac{1}{n^2 Z_2} = g_1$$

$$n^2 = 1 + Z_2/\lambda/2 = 1 + \frac{1}{\lambda/2 g_1} = 1 + \frac{1}{\lambda g_1} = 2.6$$

$$Z_1 = \frac{1}{n^2} = .382$$

$$Z_2 = \frac{1}{g_1 n^2} = .618$$

(c)



Problem 5 (50 points) Waveguides

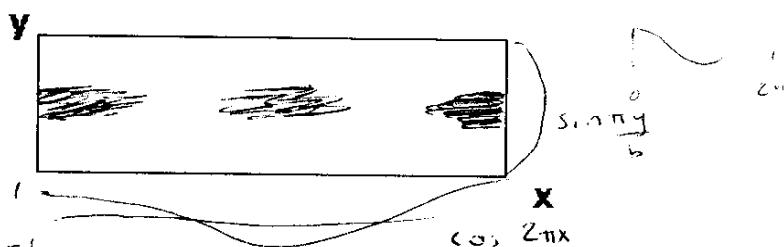
A rectangular waveguide has a cross section of 12 cm x 4 cm and is filled with ceramic that has  $\epsilon_r = 9.0$

- 10 (a) Calculate the cutoff frequencies for the first four modes.

Mode	Fc (Hz)
TE <sub>10</sub>	0.41 G
TE <sub>20</sub>	1.83 G
TE <sub>01</sub> , TE <sub>30</sub>	1.24 G
TE <sub>11</sub> , TM <sub>11</sub>	1.30 G

- 20 (b) Sketch the |Ex| for the TM<sub>21</sub> mode by shading the areas with high |Ex| dark and other areas light.

$$E_{x,TM_{21}} = K \cos \frac{2\pi x}{a} \sin \frac{\pi y}{b} e^{-j\beta z}$$



- 20 (c) Sketch a method of feeding the TM<sub>21</sub> mode using aperture coupling for the electric field that DOES NOT allow the TE<sub>21</sub> mode to be excited.

$$(a) f_c = \frac{1}{2\pi\sqrt{\mu\epsilon}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2} = 0.0158 \times 10^9 \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$\mu = 1.26 \times 10^{-6}$$

$$\epsilon = \epsilon_r \epsilon_0 = (9)(8.854 \times 10^{-12})$$

$$a = 12 \text{ cm} \quad b = 4 \text{ cm}$$

$$10 \quad .41 \text{ G}$$

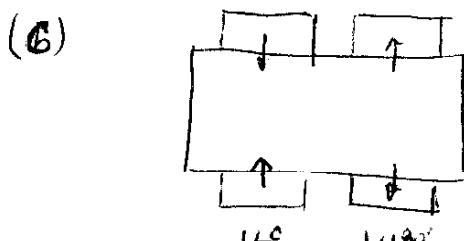
$$20 \quad .83 \text{ G}$$

$$30 \quad 1.24 \text{ G}$$

$$40 \quad 1.65 \text{ G}$$

$$11 \quad 1.30 \text{ G}$$

$$01 \quad 1.24 \text{ G}$$



For example  
(But it allows  
TE<sub>21</sub> to  
propagate)

### Problem 6 (50 points) Noise

Find the effective noise temperature of the WLAN receiver discussed in class. Consider one arm of the receiver containing an antenna, amplifier, splitter, filter, detector.

Given:

The ambient temperature is 290 K.

The antenna is a monopole with a gain of 3 (linear, not dB)

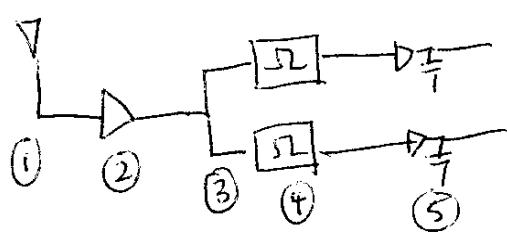
The amplifier is the only active device and has a noise temperature of 350 K. It has a gain of 15 dB.

The power divider is a 3dB splitter.

The filters are coupled line bandpass filters with a gain of -5 dB in the passband.

The diode detectors are perfectly matched (◎) and have a gain of 0 dB.

$$T_{\text{cos}} = T_{e1} + \frac{T_{e2}}{G_1} + \frac{T_{e3}}{G_1 G_2} + \frac{T_{e4}}{G_1 G_2 G_3} + \frac{T_{e5}}{G_1 G_2 G_3 G_4}$$



$$T_{e1} = 290^{\circ}\text{K} \quad G_1 = 3$$

$$T_{e2} = 350^{\circ}\text{K} \quad G_2 = 10^{\frac{15}{10}} = 31.6$$

$$T_{e3} = 290^{\circ}\text{K} \quad G_3 = 10^{-\frac{3}{10}} = 0.5$$

$$T_{e4} = 290^{\circ}\text{K} \quad G_4 = 10^{-\frac{5}{10}} = 0.316$$

$$T_{e5} = 290^{\circ}\text{K} \quad G_5 = 1.0$$

$$T_{\text{cos}} = (290) + \frac{350}{3} + \frac{290}{(3)(31.6)} + \frac{290}{(3)(31.6)(0.5)}$$

$$+ \frac{290}{(3)(31.6)(0.5)(1.0)} = \boxed{421.96^{\circ}\text{K} = T_{\text{cos}}}$$

Name \_\_\_\_\_

Problem 1 \_\_\_\_\_ / 50 points

Problem 2 \_\_\_\_\_ / 50 points

Midterm I replacement total \_\_\_\_\_

Problem 3 \_\_\_\_\_ / 50 points

Problem 4 \_\_\_\_\_ / 50 points

Midterm II replacement total \_\_\_\_\_

Problcm 5 \_\_\_\_\_ / 50 points

Problem 6 \_\_\_\_\_ / 50 points

Midterm III replacement total \_\_\_\_\_